

# Simplified-physics high frequency ground-motion simulations using site-specific parameters

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## 1 Motivation

- Accurate estimation of high-frequency ground-motion is challenging due to poor understanding of physics behind their generation and propagation.
- Broadband simulations typically use simplified physics-based approach to compute high frequency (>1 Hz) ground-motions.
- Simplified physics-based technique employ same 1D S-wave/ P-wave velocity ( $V_s/V_p$ ) and anelastic attenuation ( $Q_s/Q_p$ ) profiles for all sites (generic case).
- Objective:** Modify conventional simplified physics-based method to use site-specific information, build theoretical understanding and analyze improvements over generic approach.

## 2 Example of results for conceptual understanding

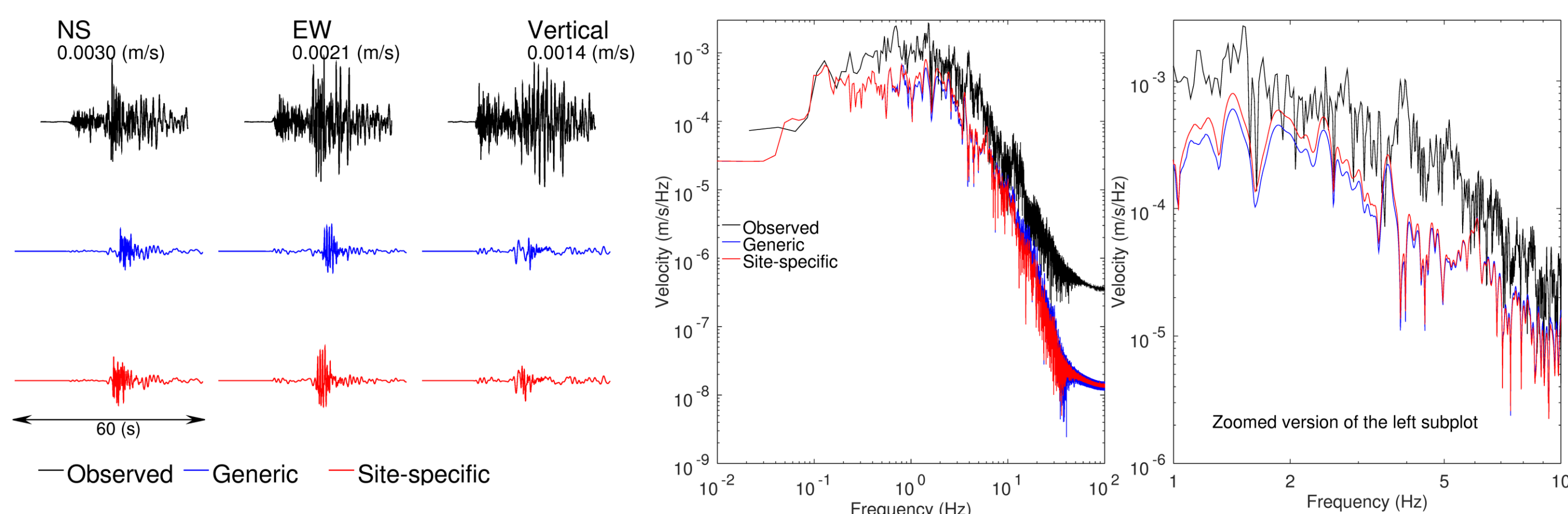


Figure 1: Waveform and Fourier spectra comparison.

- Comparing simulated ground motions from generic and site-specific approaches to recorded data due to April, 2011 (Mw 5.0) earthquake at CSHS site (which is 125 km from the source and is a 'rock' site).
- Simulations using generic approach show larger underprediction than site-specific method in predicting observations.

## 3 Concept of high-frequency computation method

- The Fourier Acceleration Spectrum (FAS) of ground-motion can be written as,
 
$$Y(M_0, R, f) = S(M_0, f) P(R, f) G(f) \quad (1)$$
 where  $S$ ,  $P$  and  $G$  represent source, path and site components of ground-motion. The site component is further subdivided into site-amplification  $A(f)$  and site-attenuation  $D(f)$ .
- The ratio of FAS while using site-specific (SS) parameters in comparison to generic (Gen) approach,
 
$$Y_{SS2Gen} = \frac{Y_{SS}}{Y_{Gen}} = \frac{S}{S} \frac{P_{SS}}{P_{Gen}} \left[ \frac{A_{SS}}{A_{Gen}} \frac{D}{D} \frac{CB14_{SS}}{CB14_{Gen}} \right] = P_{SS2Gen} A_{SS2Gen} CB14_{SS2Gen} \quad (2)$$
 where  $CB14$  represents the Campbell and Bozorgnia (2014) empirical model used to account for the near-surface non-linear soil effects.

## 4 Site-specific site-amplification $A(f)$

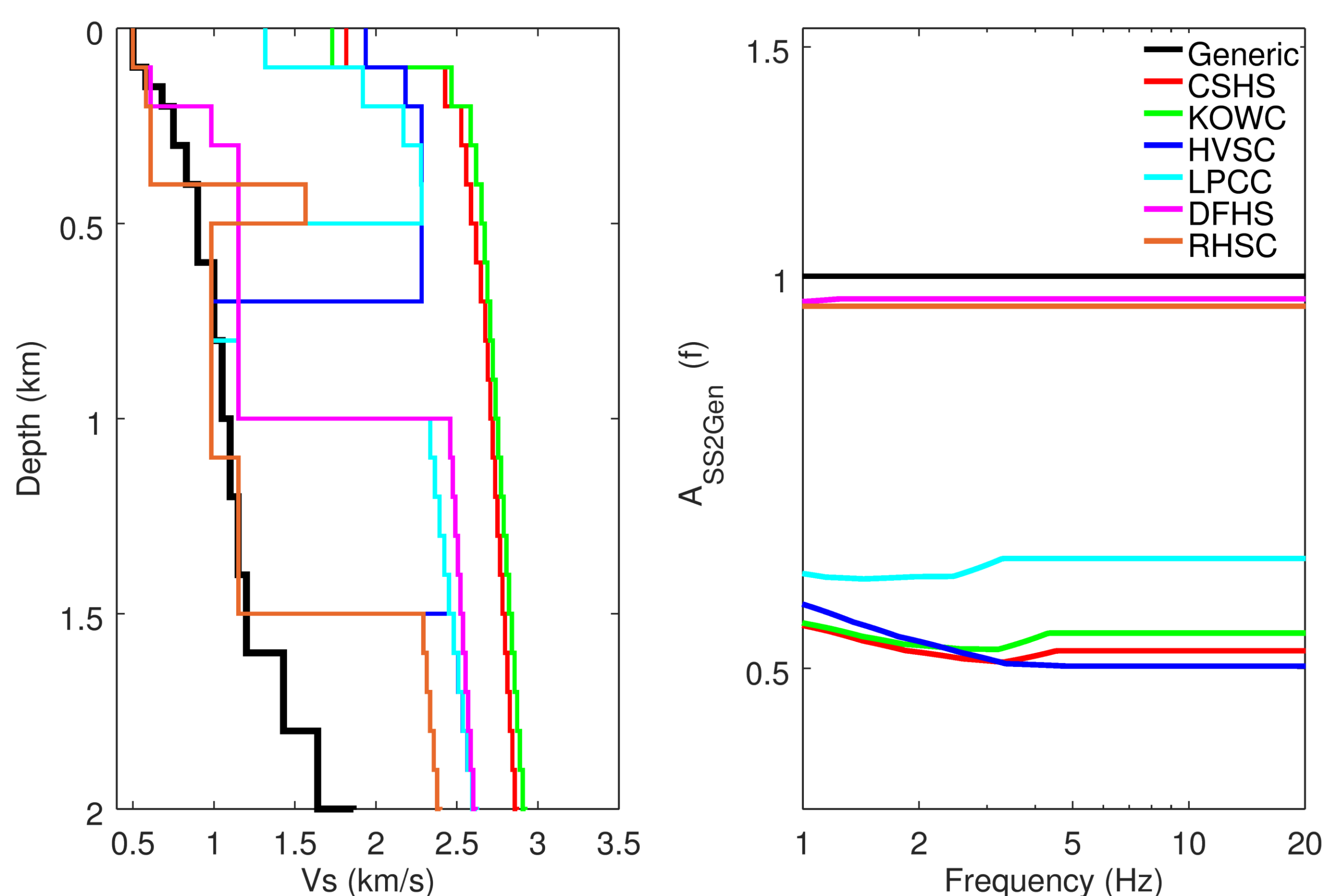


Figure 2: 1D  $V_s$ -profiles at six different sites and the ratio of site-amplification function calculated using site-specific  $V_s$  profile to generic  $V_s$  model.

- The site-amplification will be almost same for two soil sites (DFHS and RHSC) whereas ground-shaking at four rock sites will be lowered due to using site-specific  $V_s$  compared to generic  $V_s$ .

## 5 Site-specific path component $P(R, f)$

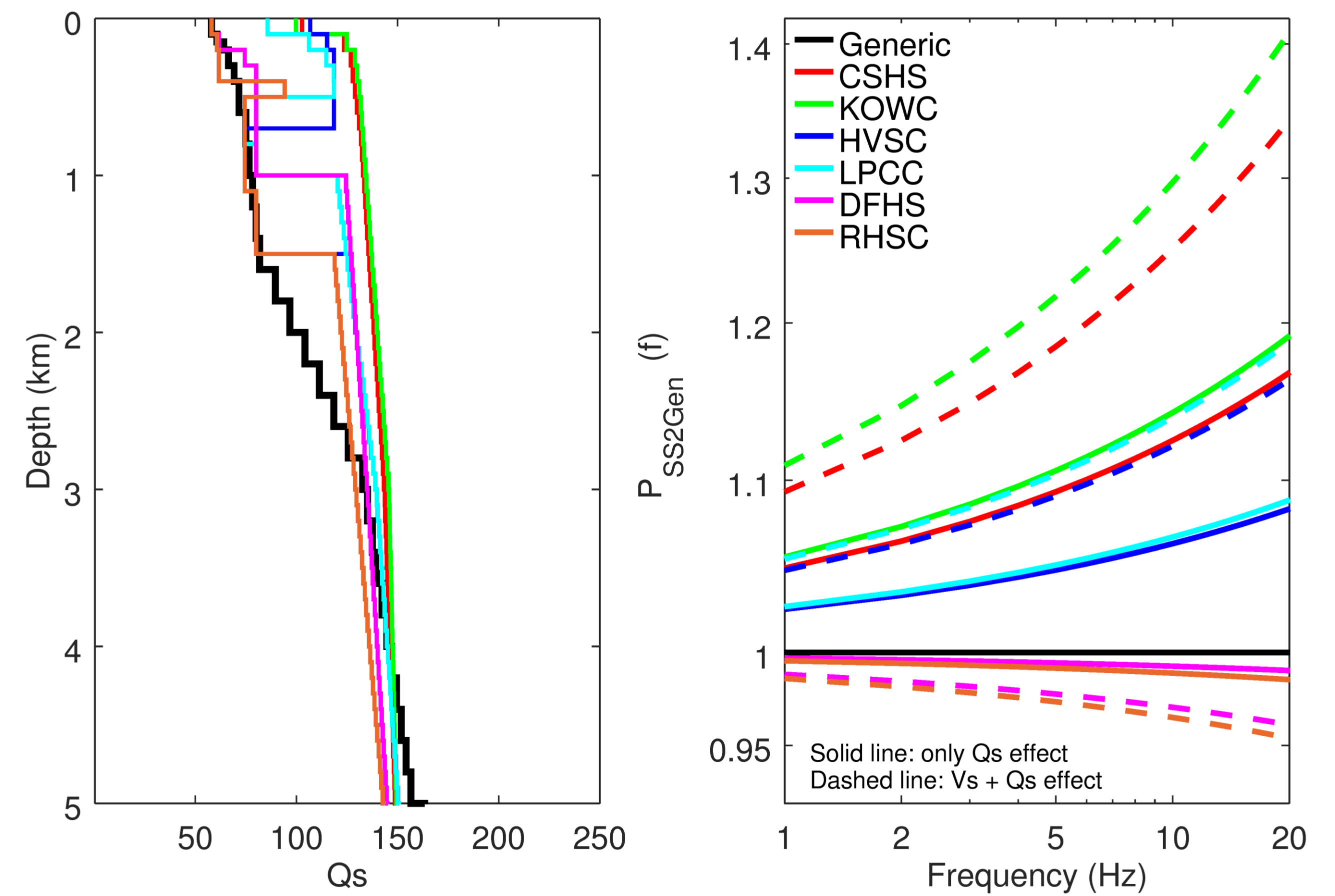


Figure 3: 1D  $Q_s$ -profiles at six different sites and the ratio of path function; solid lines – only  $Q_s$  effects; dashed lines – combined effect of  $V_s$  and  $Q_s$ .

- Theoretically the ground-motion due to path effects at four rock sites will be higher from site-specific approach than generic case whereas for soil sites it remains almost comparable or slightly lower.

## 6 Site-specific $V_{s30}$ -based amplification $CB14$

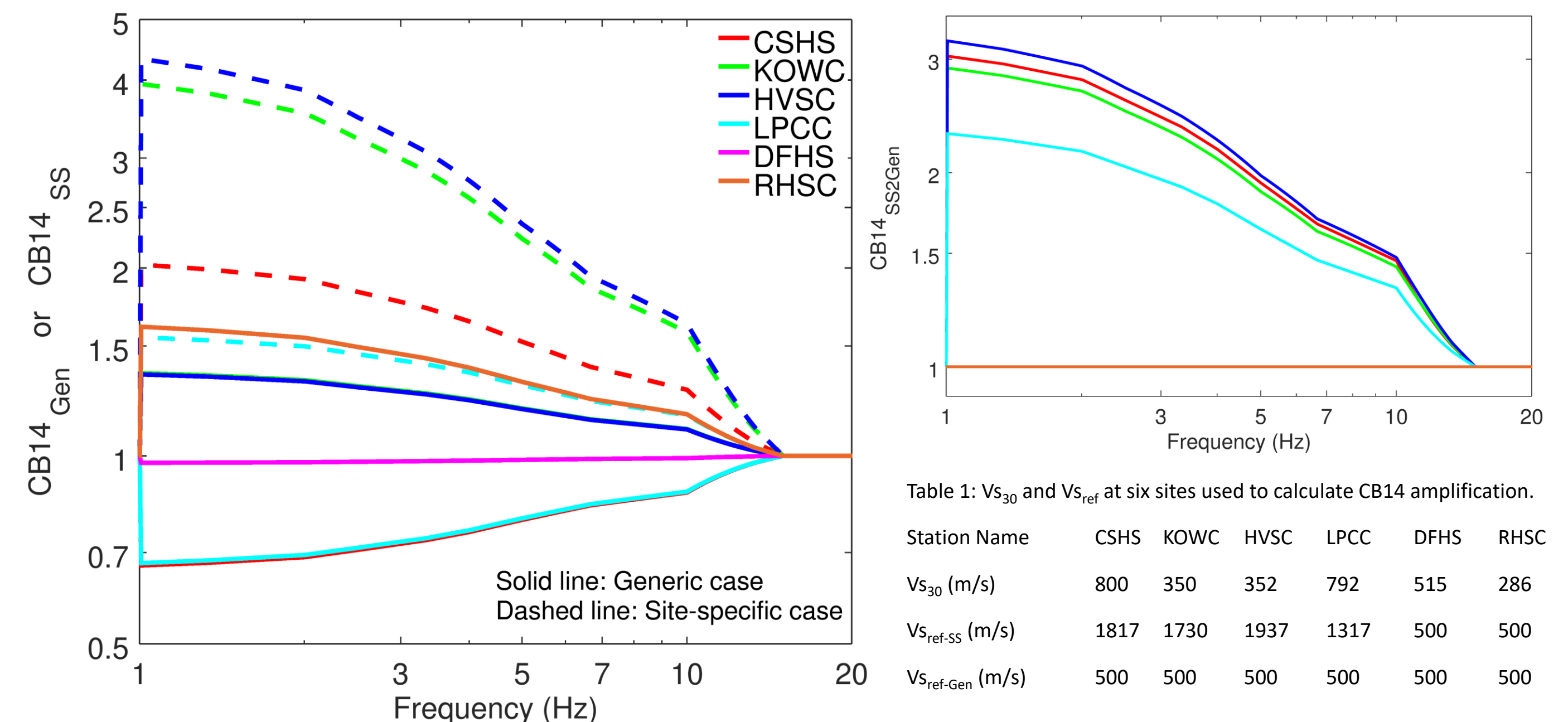
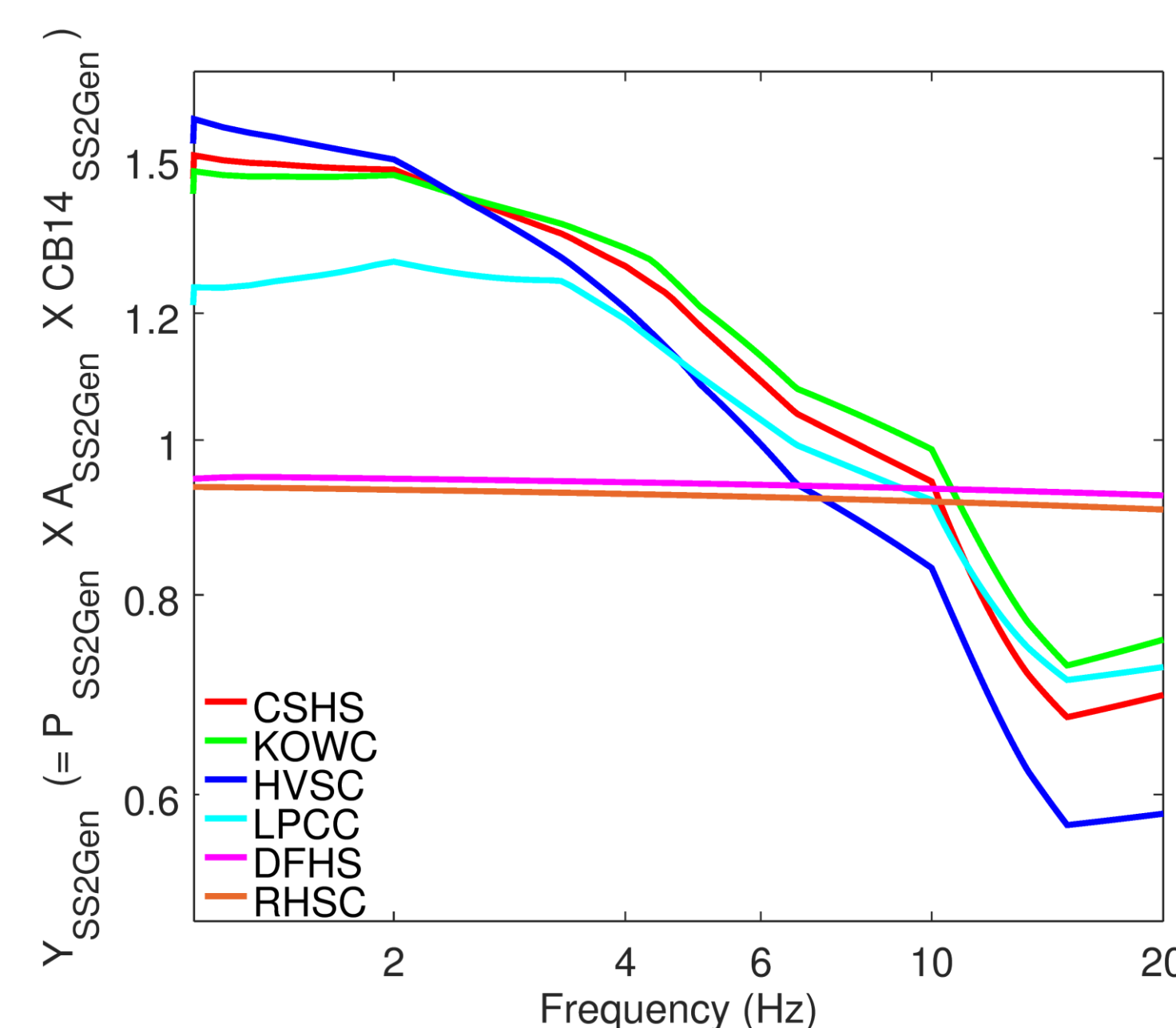


Figure 4:  $CB14$  amplification calculated for six different sites using generic and site-specific soil conditions; and corresponding ratio of  $CB14$  amplifications.

- The ground-motion at the four rock sites will be elevated for site-specific soil conditions compared to generic ones.

## 7 Site-specific Fourier Acceleration Spectrum FAS



- The FAS ratio at the four rock sites is greater than one for frequencies less than 6 Hz suggesting larger ground-motion from site-specific technique than generic approach.

Figure 5: The theoretical estimation of FAS ratio calculated using site-specific method to generic approach.

## 8 Conclusions

- We build theoretical understanding for computing high-frequency ground-motions using site-specific approach and our theoretical findings are in agreement with simulations (compare figures 5 and 1).
- The site-specific technique results in larger FAS (therefore, lower pSA residuals with respect to observed data) in comparison to generic approach (specially for rock sites).